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**Modeling Magnetostrictive Microstructure
Under Loading**

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Simulation of Magnetoelastic Systems

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Modeling Magnetostrictive Microstructure Under Loading

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and

Simulation of Magnetoelastic Systems

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$$W(RF_H, mR^T, x) = W(F, m, x) \text{ for } R \in SO(3) \text{ and } H \in H_x,$$

where H_x is the symmetry group of the material at $x \in \Omega$. In our case, H_x will be the proper cubic group H of order 24 or one of its conjugacy classes.

In Terfenol-D, onset of ferromagnetism is associated with a stretch of the high temperature cubic unit cell along a main diagonal, inducing a magnetization parallel to that diagonal. Thus the energy density W for a single crystal achieves its minimum on the eight pairs of transformation strains $(U_i, \pm m_i)$ given by

$$U_i = \eta_1 I + (\eta_2 - \eta_1) m_i \otimes m_i, \quad 0 < \eta_1 < \eta_2, \quad i = 1, 2, 3, 4, \quad (1.3)$$

$$m_1 = \frac{1}{\sqrt{3}}(1, 1, 1), \quad m_2 = \frac{1}{\sqrt{3}}(-1, 1, 1), \quad m_3 = \frac{1}{\sqrt{3}}(1, -1, 1), \quad m_4 = \frac{1}{\sqrt{3}}(1, 1, -1).$$

This leads to

$$W(RU_j, m_j R^T) = W(RU_1 H, m_1 R^T) = \min W, \quad R \in SO(3), \quad H \in H, \quad j = 1, 2, 3, 4.$$

As suggested in Figure 1, the typical configuration of $TbDyFe_2$ rods is a twinned dendritic structure consisting of lamellar domains separated by grain boundaries or growth twin interfaces. The entire rod is viewed as a composite, that we take here to be one domain $\Omega^+ = \{x \cdot m_1 > 0\} \cap \Omega$ and a second one $\Omega^- = \{x \cdot m_1 < 0\} \cap \Omega$. The lower lamellar structure arises as a rotation of 180° about the m_1 axis of the original upper lattice. Denoting by R_0 this rotation, we arrive at an energy density of the composite given by

$$W(F, m, x) = \begin{cases} W(F, m) & x \in \Omega^+ \\ W(FR_0, m) & x \in \Omega^- \end{cases} \quad (1.4)$$

Note that R_0 is not a symmetry element of the original energy and, although holding invariant the wells of $(U_i, \pm m_i)$, gives a different set of transformation strains and magnetizations $(U'_i, \pm m'_i) = (R_0 U_i, \pm m_i R_0)$.

We may now investigate the collection of twinned dendritic equilibrium structures corresponding to $H = 0$. From theory ([23, 24]), we know that a minimizing sequence (y^k, m^k) giving rise to such a configuration must satisfy

$$\int_{\Omega} W(\nabla y^k, m^k, x) dx + \frac{1}{2} \int_{\mathbb{R}^3} |\nabla_y u^k|^2 dy \rightarrow \min W | \Omega |$$

For the Young measure $v = (v_x)_{x \in \Omega}$ generated by $(\nabla y^k, m^k)$, we then have that

$$\int_{\Omega} \int_{M \times S^2} W(A, \mu, x) dv_x(A, \mu) dx = \min W | \Omega |, \text{ and} \quad (1.5)$$

$$\operatorname{div}_y \bar{m} = 0 \text{ where } \bar{m} = \int_{M \times S^2} \mu dv_x(A, \mu)$$

and M denotes the set of 3×3 matrices. This determines the variational condition for the support of the measure v , namely

$$\operatorname{supp} v_x \subset \Sigma^+ = \{(RU_i, \pm m_i R^T) : R \in SO(3), i = 1, 2, 3, 4\} \text{ for } x \in \Omega^+ \text{ and}$$

$$\operatorname{supp} v_x \subset \Sigma^- = \{(RU'_i, \pm m'_i R^T) : R \in SO(3), i = 1, 2, 3, 4\} \text{ for } x \in \Omega^- \quad (1.6)$$

The twinned dendritic laminates are the Young Measures with the simple form

$$v_x = \begin{cases} \frac{1}{2}(1 - \lambda)(\delta_{(M, m)} + \delta_{(M, -m)}) + \frac{1}{2}\lambda(\delta_{(N, q)} + \delta_{(N, -q)}) & x \in \Omega^+ \\ \frac{1}{2}(1 - \lambda')(\delta_{(M', m')} + \delta_{(M', -m')}) + \frac{1}{2}\lambda'(\delta_{(N', q')} + \delta_{(N', -q')}) & x \in \Omega^- \end{cases} \quad (1.7)$$

$$\text{where } (M, m), (N, q) \in \Sigma^+ \text{ and } (M', m'), (N', q') \in \Sigma^-.$$

We confine our attention to the deformation gradients alone. It then follows from the minors relations that we are reduced to solving an algebra problem for macroscopic deformation gradients F composed of matrices M and N and F' composed of matrices M' and N' which satisfy

$$\begin{aligned} F &= (1 - \lambda)M + \lambda N \text{ and } F' = (1 - \lambda')M' + \lambda' N', \quad 0 \leq \lambda, \lambda' \leq 1, \\ M - N &= \alpha \otimes n, \quad M' - N' = \alpha' \otimes n', \text{ and} \\ F' - F &= b \otimes m_1 \end{aligned} \quad (1.8)$$

where $(M, m), (N, q) \in \Sigma^+, (M', m'), (N', q') \in \Sigma^-$

variants	twin planes	intersection of twin plane with (0-11)
1 2	(100) twin (011) reciprocal	$\langle 011 \rangle$ $\langle 100 \rangle$
1 3	(010) twin (101) reciprocal	$\langle 100 \rangle$ $\langle -111 \rangle$
14	(001) twin (110) reciprocal	$\langle 100 \rangle$ $\langle -111 \rangle$
23	(001) twin (110) reciprocal	$\langle 100 \rangle$ $\langle 111 \rangle$
34	(-100) twin (01-1) reciprocal	$\langle 011 \rangle$ parallel to $\langle 01-1 \rangle$
24	(0-10) twin (10-1) reciprocal	$\langle 100 \rangle$ $\langle 111 \rangle$

Table 1. Twinning data for the compatible variants. The third column gives the intersection of the twin plane with the (0-11) plane of observation

The middle line above is the twinning equation for the individual laminates subject to the constraint that (1.5) holds. The transformation strains (1.3) determine a coherent well structure: any pair of wells admits two lamellar configurations, and hence 12 in all for each of Ω^+ and Ω^- . Combining these, there are 144 possible combinations satisfying the middle line of (1.8), but imposing the condition of coherence across the growth twin boundary, which is the last line of (1.8), reduces these to twelve. They must have $i = k, j$

and in this case, q is a normal direction for the interface between the two systems, either coarse or fine phase in our Young Measure sense.

The choice $q = (0,1,0)$ has the property

$$Qm_1 = -m_3 \text{ and } Qm_2 = m_4.$$

Note incidentally that since $n \cdot q = 0$, $Qn = -n$ and the normal direction is preserved. Now

$$QU_1Q = U_3 \text{ and } QU_2Q = U_4,$$

so by choosing $R^\dagger$ appropriately, we may solve (3.3). Thus a transformation path may be found and moreover, the interface normal is $(0,1,0)$, independent of the volume fraction λ . For further discussion of the compatibility between different systems of variants and connections with experiment, see Tickle [36].

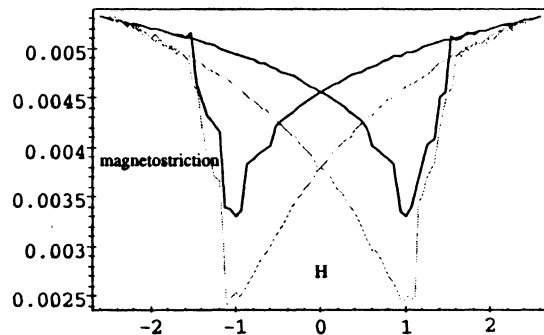


Figure 2. Computed hysteresis curves for a laminate (gray lower curve) and for a laminate with constrained growth twin interface and under compression (black upper curve).

Actual device performance under magnetic loading shows hysteretic behavior. Simulations have been employed to capture this phenomena, [27,28,29], and open the issue of the nature of metastable magnetic configurations. For a description of the experimental magnetostrictive curve we refer to Clark [14] and the references there. Metastability from the experimental, computational, and analytical points of view is an active topic of research we do not have space to review here. We wish to remark only that the ability to produce a reliable and robust hysteresis curve by applying a general numerical method, like the conjugate gradient method, to a nonconvex functional was unanticipated and has led to some new ideas for analyzing such curves.

The simulation which gives rise to Figure 2 is based on linear theory in two dimensions but includes the magnetostatic energy term. The curve corresponding to the constrained growth twin interface more closely resembles the experimental picture, suggesting a role for the growth twin in the magnetostrictive process which to date is not clearly understood.

On the other hand, the width of the hysteresis loop seems to be relatively insensitive to loading or constraints. Indeed, additional simulations under a wide variety of conditions, for example, without magnetic field energy or elasticity or single crystals with magnetic field energy, suggest that the width of the curve is extremely robust. The simulation which

gives Figure 2 is the first, to our knowledge, where competition between magnetic and elastic effects is prominent.

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Simulation of Magnetoelastic Systems

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Abstract The simulation of a magnetoelastic system subjected to magnetic field loading gives rise to hysteresis. Examples related to Terfenol-D are presented and some methods of analysis discussed.

KEYWORDS magnetoelastic system, Terfenol-D, simulation, magnetostriction, metastability, micromagnetic theory

1. Introduction

We discuss the simulation of the behavior of a magnetoelastic system under magnetic field loading. Our principle objective is to understand the magnetostrictive curve of Terfenol-D, $\text{Tb}_x\text{Dy}_{1-x}\text{Fe}_2$, $x \approx 0.3$, from the viewpoint of micromagnetic theory, [3,4,9,14,15-19]. Simulations of magnetic, magnetostrictive, and pseudoelastic behavior exhibit hysteresis, [20-23]. These systems have a highly nonlinear character involving both short range anisotropy and elastic fields and dispersive demagnetization fields. The hysteretic character of a simple system that moves quasistatically is robust. The energy profile in terms of applied magnetic field, and in particular, the width of the hysteresis loop, is invariant under mesh refinement. This is true even in the absence of an imposed dynamical mechanism, like the Landau-Lifschitz-Gilbert equation. This permits us, for example, to extract useful information by computing on fairly coarse grids. It is also very efficient, running at an excess of 200 MFLOPS on the Pittsburgh Supercomputing Center Cray C90. A typical simulation involves 600 to 800 field steps, each one of which represents a complete conjugate gradient iteration procedure. For experimental observations and theory we refer to [1,2,5-7,13]. Instabilities in Terfenol films are studied in Wurtig et al. [27].

An important feature of this type of simulation is that computed states are only metastable. Indeed, since the energy of configurations on loading and unloading are different for the same value of the imposed magnetic field, not both and usually neither can be minima. Little is known to guide us about metastability in this context. In addition, Terfenol displays a complicated lamellar microstructure whose role in the magnetostrictive process remains under investigation, [26]. Although confirming our ability to determine general features of the magnetization and magnetostriction, our results do not accurately describe the microstructure. So there is much room for improvement. However, we would like to point out that in our attempts to account for behavior of the growth twin midrib in our laminate, we witness a wave of magnetization reversal propagate across the domain. This is first evidence that we are able to achieve some progress here.

We have developed a model to understand the metastability in the computation. Let us explain the basis of this model with the comment that we have attempted to confine ourselves to what we perceived the strategic essentials: a stored energy of deformation and magnetization, a demagnetization or induced magnetic field energy, and a simple magnetic loading program intended to represent behavior when a device is subjected to a slowly oscillating field, e.g., 60 Hz. If there were no demagnetization field, one would anticipate the evolution of the system to resemble that of a single magnetic particle, as described by Stoner and Wohlfarth [25]. Our idea is to derive a shadow energy that will accumulate the effects of the oscillatory behavior resulting from the demagnetization field. Although the mathematics involved here is elementary, beyond some knowledge of modern partial differential equations, the idea is that the shadow energy serves as a model of the complex simulation, just as formulating balance laws or energy principles serves as model for a physical process.

We introduce a two dimensional energy density based on a three dimensional linear elastic density with magnetic easy axes parallel to the $\langle 111 \rangle$ directions. The three dimensional density is projected onto the $(0-11)$ plane containing the $[-211]$ rod axis. Then we ignore out of plane strains and magnetizations. Note that the $[111]$ and $[-111]$ easy axes lie in the plane of projection. After performing these computations, we relabel axes in our two dimensional configuration so that $e_1 = (1,0)$ and $e_2 = (0,1)$ correspond to the $[111]$ and $[-211]$ directions. In these coordinates, the $[111]$ easy axis becomes e_2 and the $[-111]$ easy axis becomes $q = (\frac{2\sqrt{2}}{3}, \frac{1}{3})$. Set

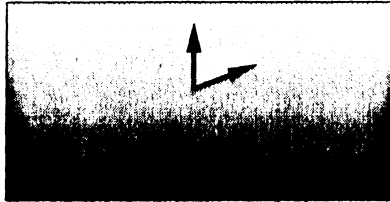


Figure 1a Single crystal with magnetic easy axes.

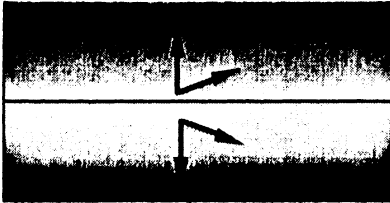


Fig 1b Growth twin laminate with magnetic easy axes.

(ii) *single crystal with demagnetization energy* The configuration destabilizes from the precursor prior to H_{1cr} and descends gradually through the shoulder regime achieving absolute minimum slightly after H_{2cr} .

(iii) *growth twin laminate with demagnetization energy* The configuration destabilizes from the precursor subsequent to passing the field value H_{1cr} achieving absolute minimum slightly beyond H_{2cr} .

(iv) *growth twin laminate with demagnetization energy and constrained growth twin boundary* The general features are the same as in (iii) with a somewhat smoother ascent to H_{2cr} . The magnetostrictive strain is diminished.

We are able to provide a qualitative comparison with experiment. Material parameters useful for a more detailed comparison are not available. The computed curves in Figure 2

bear a strong resemblance to the experimental curve [6]. The strain increases with increasing positive and negative applied field and has the butterfly structure characteristic of this material. The λ -jumping described in [2] is evident in the steep section of the curve, although this is less pronounced in the experimental picture. In [7], an unbiased rod achieves about 66% of its maximum magnetostrictive strain according to one of the authors. In our simulation we achieve about 50%, which leads us to believe that our choices of parameters are reasonable.

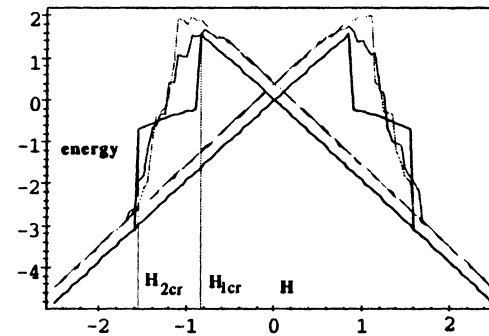


Figure 2. Energy portraits: without demagnetization energy (lowest curve), single crystal with demagnetization energy (intermediate curve), and laminate with demagnetization energy (top curve). Critical fields are labeled.

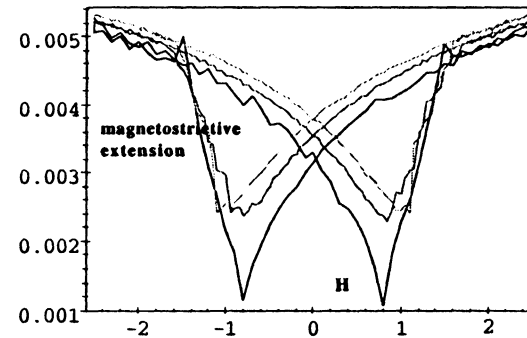


Figure 3. Magnetostriction curves: without demagnetization energy (lowest curve), single crystal with demagnetization energy (intermediate curve), and laminate with demagnetization energy (top curve).

Let α^0 be a given magnetization, perhaps depending on H or other parameters, and let $\alpha^h = \alpha^0 \chi_\Omega + (\xi - \alpha^0) \chi_D$, $|\xi| = 1$, $D = (0, h) \times (0, 1) \cup (L-h, L) \times (0, 1)$, (3.1) where $h > 0$, be a variation of α^0 . We shall interpret α^0 as a suitably stable precursor.

The energy of the system is given by

$$E(H, \alpha) = E(H, \alpha^0) + |D| \frac{E(H, \alpha) - E(H, \alpha^0)}{|D|}.$$

Our shadow energy E_Δ is given by

$$E_\Delta(H, \alpha^0, \xi) = E(H, \alpha^0) + \Psi^0(H, \alpha^0, \xi) |D|, \quad (3.2)$$

$$\Psi^0(H, \alpha^0, \xi) = \lim_{h \rightarrow 0} \frac{E(H, \alpha) - E(H, \alpha^0)}{|D|} = \lim_{h \rightarrow 0} \Psi^h(H, \alpha^0, \xi), \text{ where}$$

$$\Psi^h(H, \alpha^0, \xi) = \varphi(\xi) - \varphi(\alpha^0) - H(\xi - \alpha^0) + \frac{1}{2h} \frac{1}{2} \int_{R^2} (|\nabla u|^2 - |\nabla u^0|^2) dx, \quad (3.3)$$

with

$$\Delta u = \operatorname{div} \alpha^h \chi_\Omega \text{ in } R^2 \text{ and } \Delta u^0 = \operatorname{div} \alpha^0 \chi_\Omega \text{ in } R^2.$$

The essence of the problem is to evaluate with care the demagnetization term. Note that from the differential equation we obtain that

$$\int_{R^2} (|\nabla u|^2 - |\nabla u^0|^2) dx = \int_D \nabla(u + u^0) \cdot (\xi - \alpha^0) dx$$

We suppose α^0 and ξ to be independent of $x \in D$. Introduce the auxiliary functions w_j and $v_j^{(h)}$ as the solutions of the equations

$$\Delta w_j = \frac{\partial}{\partial x_j} \chi_\Omega \text{ and } \Delta v_j^{(h)} = \frac{\partial}{\partial x_j} \chi_D \text{ in } R^2, \quad j = 1, 2.$$

Moreover, we shall need explicit representations for $\partial w_j / \partial x_1$ and $\partial v_j^{(h)} / \partial x_1$. These are given by the classical Plemelj formulas [24]. Namely, in the case at hand, if w denotes the solution of

$$\Delta w = \frac{\partial}{\partial x_1} \chi_A \text{ in } R^2, \text{ where } A \text{ is a rectangle with sides } \parallel \text{ to the axes,}$$

then $(z = x_1 + ix_2)$,

$$\frac{\partial w}{\partial z}(z) = \frac{1}{2\pi i} \int_{\Gamma_1 \cup \Gamma_2} \frac{dt}{t - z}, \text{ where } \Gamma_1 \text{ and } \Gamma_2 \text{ are the vertical sides.}$$

So

$$\frac{\partial w}{\partial x_1}(z) = \operatorname{Re} \frac{1}{2\pi i} \int_{\Gamma_1 \cup \Gamma_2} \frac{dt}{t - z} = \frac{1}{2\pi} (\theta_1(z) + \theta_2(z)), \quad (3.4)$$

where $\theta_j(z)$ is the angle subtended by z and Γ_j .

Returning to (3.3), we express the field potential

$$u = u^0 + (\xi_1 - \alpha_1^0) v_1^{(h)} + (\xi_2 - \alpha_2^0) v_2^{(h)} \quad (3.5)$$

which, after some manipulation, gives that

$$\begin{aligned} \nabla(u + u^0) \cdot (\xi - \alpha^0) &= 2\alpha_1^0 (\xi_1 - \alpha_1^0) \frac{\partial w_1}{\partial x_1} + 2\alpha_2^0 (\xi_2 - \alpha_2^0) \frac{\partial w_2}{\partial x_2} \\ &+ (\xi_1 - \alpha_1^0)^2 \frac{\partial v_1^{(h)}}{\partial x_1} + (\xi_2 - \alpha_2^0)^2 \frac{\partial v_2^{(h)}}{\partial x_2} + I, \text{ where } \int_D I dx = 0, \end{aligned}$$

by symmetry. From (3.4) we observe that

$$\lim_{h \rightarrow 0} \frac{1}{|D|} \int_D \frac{\partial v_1^{(h)}}{\partial x_1} dx = 1 \quad \text{and} \quad \lim_{h \rightarrow 0} \frac{1}{|D|} \int_D \frac{\partial v_2^{(h)}}{\partial x_2} dx = 0.$$

We introduce a domain dependent "magic number" λ by

$$\lambda = \int_{\Gamma_1} \frac{\partial w_1}{\partial x_1} dx_2 = \lim_{h \rightarrow 0} \frac{1}{|D|} \int_D \frac{\partial w_1}{\partial x_1} dx, \quad (3.6)$$

so in particular, by (3.4) again,

$$1 - \lambda = \int_{\Gamma_1} \frac{\partial w_2}{\partial x_2} dx_2 = \lim_{h \rightarrow 0} \frac{1}{|D|} \int_D \frac{\partial w_2}{\partial x_2} dx.$$

We then obtain for the demagnetization portion of the shadow energy,

$$\begin{aligned} \Psi_{\text{demag}}^0(H, \alpha^0, \xi) &= \lim_{h \rightarrow 0} \frac{1}{|D|} \frac{1}{2} \int_{R^2} (|\nabla u|^2 - |\nabla u^0|^2) dx \\ &= \alpha_1^0 (\xi_1 - \alpha_1^0) \lambda + \alpha_2^0 (\xi_2 - \alpha_2^0) (1 - \lambda) + \frac{1}{2} (\xi_1 - \alpha_1^0)^2 \end{aligned} \quad (3.7)$$

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